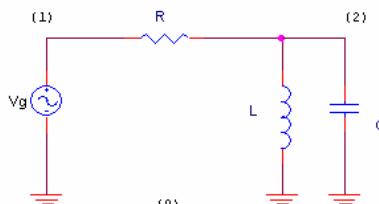


Circuit rezonant – LC paralel

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Scopul lucrarii

In lucrarea de fata ne propunem analiza unui circuit liniar de tip Trece Banda (TB) de ordin II cu grupare paralel bobina si condensator. Schema circuitului este:



Descrierea circuitului

> **restart:with(Syrup):**

Descrierea circuitului folosind un netlist de tip spice:

> **FTB :=**

"filtru trece banda

Vg 1 0

R 1 2

L 2 0

C 2 0

.end":

Ecuatii de stare

> **restart:with(Syrup):FTB := "filtru trece banda\nVg 1 0\nR 1
2\nL 2 0\nC 2 0\n.end":**

Circuit rezonant LC

Descrierea folosind ecuatii de stare a circuitului

1) **ecuatie de stare (vectorial):**

> **syrup(FTB, tran, 'curenti','tensiuni');**

$$\{ v_C(0)=0, i_L(0)=0, \frac{\partial}{\partial t} v_C(t) = -\frac{i_L(t)R - Vg + v_C(t)}{CR}, \frac{\partial}{\partial t} i_L(t) = \frac{v_C(t)}{L} \}, \\ \{ v_C(t), i_L(t) \}$$

2) **ecuatii de iesire** se pot scrie in functie de tensiunile de noduri si curentii prin laturi:

> **tensiuni;**

$$\{ v_1 = Vg, v_2 = v_C(t) \}$$

> **curenti;**

$$\{ i_L = i_L(t), i_{Vg} = -\frac{Vg - v_C(t)}{R}, i_R = \frac{Vg - v_C(t)}{R}, i_C = -\frac{i_L(t)R - Vg + v_C(t)}{R} \}$$

Obs: Ordinul circuitului este egal cu 2. Descrierea functionarii circuitului se face cu un sistem de 2 ecuatii diferențiale de ordin I. Variabilele de stare sunt: tensiunea pe condensator si curentul prin bobina. In functie de aceste variabile se exprima curentii si tensiunile din circuit.

Ecuatii TTN

> **restart:with(Syrup):FTB := "filtru trece banda\nVg 1 0\nR 1
2\nL 2 0\nC 2 0\n.end":**

Descrierea circuitului folosind Teorema Tensiunilor Nodale:

> **syrup(FTB, ac, 'curenti','tensiuni');**

> **tensiuni;**

$$\{ v_2 = \frac{sL Vg}{s^2 CLR + R + sL}, v_1 = Vg \}$$

> **curenti;**

$$\left\{ \begin{array}{l} i_L = \frac{Vg}{s^2 CLR + R + sL}, i_{Vg} = -\frac{Vg(s^2 CL + 1)}{s^2 CLR + R + sL}, i_R = \frac{Vg - \frac{sL Vg}{s^2 CLR + R + sL}}{R}, \\ i_C = \frac{s^2 CL Vg}{s^2 CLR + R + sL} \end{array} \right.$$

Calculul functiei de transfer H(s)

Functia de transfer a unui sistem liniar se poate calcula prin mai multe metode:

Metoda I: divizor de tensiune

Calculul functiei de transfer folosind divizor de tensiune:

$$H(s) = \frac{sL \parallel \frac{1}{sC}}{R + \left(sL \parallel \frac{1}{sC} \right)} = \frac{s \frac{1}{RC}}{s^2 + s \frac{1}{RC} + \frac{1}{LC}}$$

Notam:

$$2a = \frac{1}{RC}, \quad w_0^2 = \frac{1}{LC}$$

Deci functia de transfer devine:

$$H(s) = \frac{2as}{s^2 + 2as + w_0^2}$$

Se defineste factorul de calitate :

$$Q = \frac{w_0}{2a}$$

In cazul nostru factorul de calitate este:

$$Q = R \sqrt{\frac{C}{L}}$$

Se calculeaza polii si zerourile functiei de transfer.

zeroi

$$z = 0$$

poli:

$$\begin{aligned} p_1 &= -a - \sqrt{a^2 - w_0^2} \\ p_2 &= -a + \sqrt{a^2 - w_0^2} \end{aligned}$$

In functie de factorul de calitate Q avem doua cazuri:

Cazul I ($Q < \frac{1}{2}$) avem doi poli reali distincti.

Cazul II: ($Q = \frac{1}{2}$) avem un pol dublu.

Cazul III ($Q > \frac{1}{2}$) avem poli complexi conjugati.

Metoda II: ecuatii TTN

Pentru circuitul cu nodurile din figura se scrie TTN:

$$\begin{cases} V_{10}(s) = Vg(s) \\ -GV_{10}(s) + \left(G + \frac{1}{sL} + sC \right) V_{20}(s) = 0 \end{cases}$$

In urma calculelor obtinem aceeasi functie de transfer ca si prin metoda I:

$$H(s) = \frac{2as}{s^2 + 2as + w_0^2}$$

Metoda III: folosind calcul simbolic

Folosind Maple si pachetul Syrup se descrie circuitul

```
> restart:with(Syrup):FTB := "filtru trece sus\nVg 1 0\nR 1 2\nL
2 0\nC 2 0\nn.end":
> libname:="c:/maple//SCSlib",libname:
> syrup(FTB, ac, 'currenti','tensiuni'):
> Hs:=eval(v[2]/v[1],tensiuni);
> Hs:=sort(simplify(eval(Hs,[C=1/(2*R*alpha),
L=(2*R*alpha)/(omega0^2)])),s);
```

$$Hs := \frac{sL}{s^2 C L R + R + sL}$$

$$Hs := 2 \frac{\alpha s}{s^2 + 2 \alpha s + \omega_0^2}$$

Zerourile functiei de transfer:

```
> z:=solve(numer(Hs)=0,s);
z := 0
```

Polii functiei de transfer:

```
> p:={solve(denom(Hs)=0,s)};
p := { -\alpha + \sqrt{\alpha^2 - \omega_0^2}, -\alpha - \sqrt{\alpha^2 - \omega_0^2} }
```

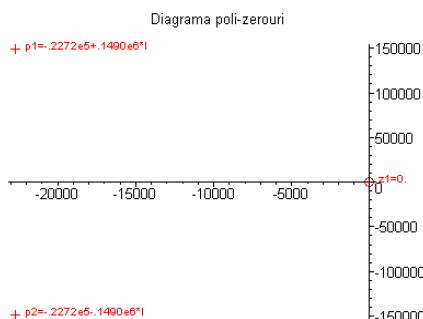
Evaluare numERICA:

```
> alpha:=1/(2*R*C):omega0:=1/sqrt(L*C):
> H:=eval(Hs,[L=0.002, C=22*1E-9, R=1000]):
```

Polii si zerourile functiei de transfer:

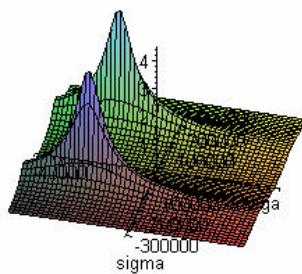
```
> PZ[numeric](H,s);
[ zI 0.
  p1 -22720. + 149000. I
  p2 -22720. - 149000. I ]
```

```
> PZ[grafic](H,s);
```



Interpretarea functiei de transfer:

```
> plot3d(abs(eval(H,s=sigma+I*omega)),sigma=-50000..50000,omega=-300000..300000,numpoints=2500,axes=normal,title="Reprezentarea in spatiu a modulului F.D.T.");
plot3d(argument(eval(H,s=sigma+I*omega)),sigma=-50000..50000,
omega=-300000..300000,numpoints = 2500,axes=normal,
title="Reprezentarea in spatiu pentru argumentul F.D.T.");
Reprezentarea in spatiu a modulului F.D.T.
```



Functia de transfer in regim permanent $H(j\omega)$

```
> restart:with(Syrup):
> libname:="~/SCSlib","~/DCElib",libname:
```

```
> Hs:=(2*alpha*s)/(s^2+2*alpha*s+omega0^2);

$$Hs := 2 \frac{\alpha s}{s^2 + 2 \alpha s + \omega_0^2}$$

> Homega:=subs(s=I*omega,Hs);

$$Homega := \frac{2 I \alpha \omega}{-\omega^2 + 2 I \alpha \omega + \omega_0^2}$$

```

Valori ale functiei de transfer $H(j\omega)$ pentru $\omega = \{0, \omega_0, \infty\}$:

```
> H0:=limit(Homega,omega=0);Hinf:=limit(Homega,omega=infinity);
abs_Homega0:=abs(simplify(eval(Homega,omega=omega0)));
arg_Homega0:=argument(simplify(eval(Homega,omega=omega0)));
H0 := 0
```

$$Hinf := 0$$

$$abs_Homega0 := 1, arg_Homega0 := 0$$

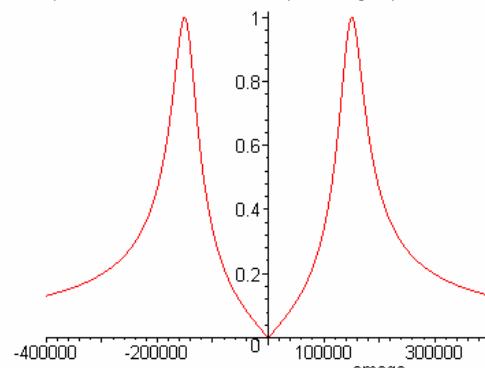
```
> alpha:=1/(2*R*C):omega0:=1/sqrt(L*C):
```

Pulsatia de rezonanta:

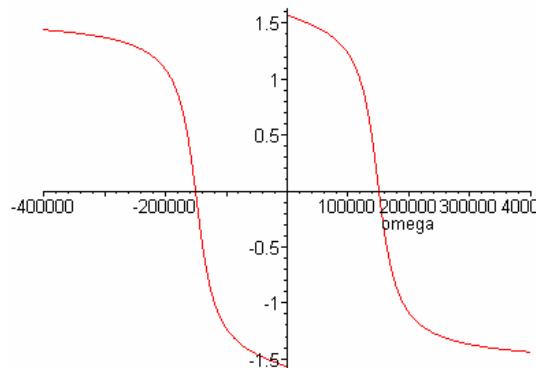
```
> val_omega0:=eval(omega0,[L=0.002, C=22*1E-9, R=1000]);
val_omega0 := 150755.6723
```

```
> plot(abs(eval(Homega,[L=0.002, C=22*1E-9, R=1000])), omega=-400000..400000,numpoints=200,axes=normal,title="Reprezentarea modulului F.D.T. pentru regim permanent");
plot(argument(eval(Homega,[L=0.002, C=22*1E-9, R=1000])), omega=-400000..400000,numpoints=200,axes=normal,title="Reprezentarea argumentului F.D.T. pentru regim permanent");
```

Reprezentarea modulului F.D.T. pentru regim permanent

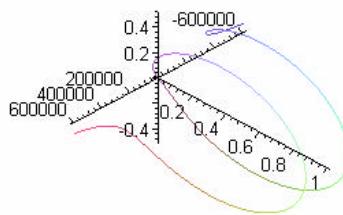


Reprezentarea argumentului F.D.T. pentru regim permanent



```
> plots[spacecurve]([omega,Re(eval(Homega,[L=0.002, C=22*1E-9, R=1000])),Im(eval(Homega,[L=0.002, C=22*1E-9, R=1000])),omega=-600000..600000],numpoints = 10000,axes=normal,
```

```
title="Reprezentarea spatiala a F.D.T. pentru regim permanent" );
Reprezentarea spatiala a F.D.T. pentru regim permanent
```



Diagrame frecventiale

```
> restart:libname:="c://maple//SCSlip","..../DCElib",libname:
> Hs:=(2*alpha*s)/(s^2+2*alpha*s+omega0^2);

$$Hs := 2 \frac{\alpha s}{s^2 + 2 \alpha s + \omega_0^2}$$

> alpha:=1/(2*R*C):omega0:=1/sqrt(L*C):
> H:=eval(Hs,[L=0.002, C=22*1E-9, R=1000]):
> cat("omega0 = ",convert(eval(omega0,[L=0.002, C=22*1E-9,
R=1000]),string)," rad/s");
"omega0 = 150755.6723 rad/s"
```

```
> Bode[castig](H,numarpunche=400);Bode[faza](H,numarpunche=400);
Diagrama Bode de castig
```

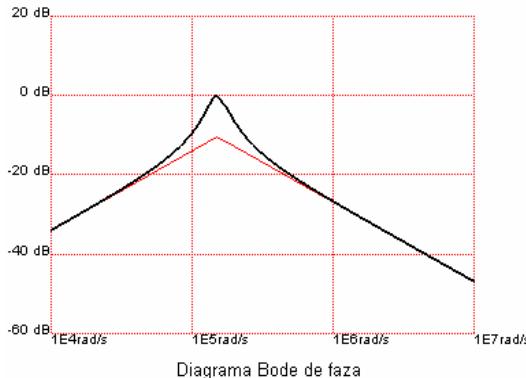
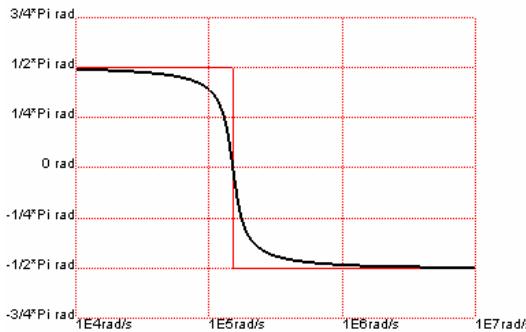


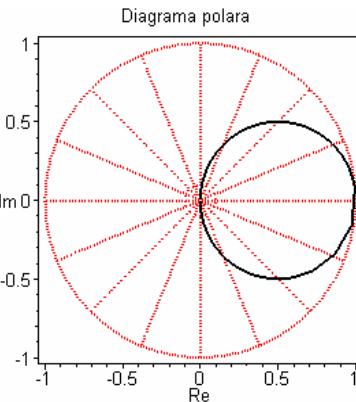
Diagrama Bode de faza



```
>cat("H(10^4)=",convert(20*log10(abs(eval(H,s=I*10^4))),string),"dB");
cat("arg(H(10^4))=",convert(argument(eval(H,s=I*10^4)),string),"grade");
"H(10^4)=-33.94285006dB"
```

"arg(H(10^4))=1.550710639grade"

> **Bode[polara](H,numarpuncte=600);**



Forma functiei de transfer la variatia pozitiei polilor

Pozitia polilor se modifica la modificarea valorii rezistentei R. Valoarea frecventei de rezonanta ramane constanta.

```
> z:=solve(numer(eval(subs(s=I*omega,Hs),[L=0.002, C=22*1E-9]))=0,omega):
> p:=solve(denom(eval(subs(s=I*omega,Hs),[L=0.002, C=22*1E-9]))=0,omega):
> plots[animate]({[(evalf(Im(p[1])),evalf(Re(p[1])))],[(evalf(Im(p[2])),evalf(Re(p[2])))]},R=50..800,frames=750,style=point):
plots[animate]([log10(omega),20*log10(abs(eval(subs(s=I*omega,Hs),[L=0.002, C=22*1E-9])))),omega=10^4..10^7],R=50..2000,frames=75, numpoints=750, title="Diagrama de cistig"):
plots[animate]([log10(omega),argument(eval(subs(s=I*omega,Hs),[L=0.002, C=22*1E-9]))),omega=10^4..10^7],R=50..2000,frames=75, numpoints=750, title="Diagrama de faza"):
```

Raspuns de regim permanent

Pentru calculul raspunsului permanent se prefera efectuarea calculelor in domeniul frecventa (din motive de simplitate – convolutia din domeniul timp se inlocuieste cu produs in domeniul frecventa)

$$1) \quad e(t) \rightarrow E(\omega) = F\{e(t)\}$$

$$2) \quad Y(\omega) = E(\omega)H(\omega)$$

$$3) \quad y(t) = F^{-1}\{Y(\omega)\}$$

```
> restart:libname:="c://maple//SCSlib",libname:
> F:=table([dir=inttrans[fourier],inv=inttrans[invfourier]]):
> Hs:=(2*alpha*s)/(s^2+2*alpha*s+omega0^2);

$$Hs := 2 \frac{\alpha s}{s^2 + 2 \alpha s + \omega_0^2}$$

> Homega:=subs(s=I*omega,Hs);

$$Homega := \frac{2 I \alpha \omega}{-\omega^2 + 2 I \alpha \omega + \omega_0^2}$$

```

Raspunsul la semnal armonic

In acest caz expresia excitatia $e(t)$ este de forma:

Circuit rezonant LC

```
> e:=A0*cos(w*t);  
e := A0 cos(w t)
```

Transformata Fourier a excitatiei $e(t)$ este:

```
> E:=F[dir](e,t,omega);  
E := A0 (\pi Dirac(-\omega + w) + \pi Dirac(\omega + w))
```

Transformata Fourier a excitatiei $y(t)$ este:

```
> Y:=Homega*E;  
Y := \frac{2 I \alpha \omega A0 (\pi Dirac(-\omega + w) + \pi Dirac(\omega + w))}{-\omega^2 + 2 I \alpha \omega + \omega_0^2}
```

Raspunsul $y(t)$ al circuitului la excitatia $e(t)$ este:

```
> y:=simplify(normal(convert(F[inv](Y,omega,t),trig),expanded));  
y := 2 \frac{\alpha A0 w (w^2 \sin(w t) + 2 \alpha w \cos(w t) - \omega_0^2 \sin(w t))}{w^4 - 2 w^2 \omega_0^2 + 4 \alpha^2 w^2 + \omega_0^4}
```

Obs: Formula de mai sus poate fi obtinuta si astfel. Se porneste de la functia de transfer $H(jw)$:

$$H(jw) = \frac{2aw}{-w^2 + 2aw + w_0^2}$$

Se calculeaza modulul si argumentul:

$$\begin{cases} |H(jw)| = \frac{2aw}{\sqrt{(w_0^2 - w^2)^2 + (2aw)^2}} \\ \arg(H(jw)) = \frac{p}{2} - \arctg \frac{2aw}{w_0^2 - w^2} \end{cases}$$

Raspunsul permanent este:

$$\begin{aligned} y(t) &= A_0 |H(jw)| \cos(wt + \arg(H(jw))) \\ y(t) &= A_0 \frac{2aw}{\sqrt{(w_0^2 - w^2)^2 + (2aw)^2}} \cos\left(wt + \frac{p}{2} - \arctg \frac{2aw}{w_0^2 - w^2}\right) \end{aligned}$$

Raspunsul la semnal armonic de frecventa de rezonanta a filtrului

Se calculeaza raspunsul circuitului la frecventa egala cu frecventa de rezonanta a filtrului:

```
> e1:=eval(e,w0=omega0);  
e1 := A0 cos(\omega0 t)
```

```
> y1:=simplify(eval(y,w0=omega0));  
y1 := A0 cos(\omega0 t)
```

Comportarea circuitului in jurul frecventei de rezonanta

Pentru circuitul fizic s-au facut notatiile:

```
> alpha:=1/(2*R*C):omega0:=1/sqrt(L*C):
```

Pulsatia de rezonanta a circuitului este:

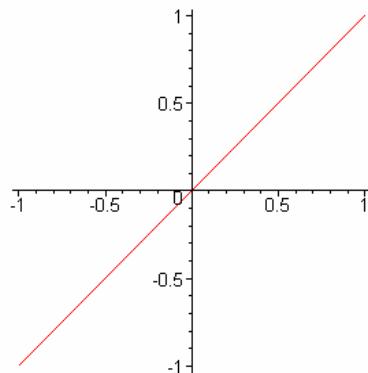
```
> omega0_val:=eval(omega0, [L=0.002, C=22*1E-9, R=1000]);  
omega0_val := 150755.6723
```

Figura Lissajoux la frecventa de rezonanta a circuitului devine o dreapta:

```
> plot(eval([e1,y1,t=-1/omega0_val*pi..1/omega0_val*pi],[L=0.002,  
C=22*1E-9, R=1000,A0=1]),title="Figura Lissajoux la frecventa de
```

taiere a filtrului");

Figura Lissajoux la frecventa de taiere a filtrului



Vom urmarii modul in care se modifica semnalul de iesire din circuit (si figura Lisajoux) la variatia frecventei semnalului de intrare. Se alege o variație a frecvenței în jurul valorii frecvenței de rezonanță.

```
> wd:=omega0_val*evalf([seq(10^(i/20),i=-10..10)]):
>INTERFACE_PLOT(ANIMATE(seq([CURVES(op(op(plot(eval(e,[A0=1,w0=wd[i]]),t=-
Pi/wd[1]..Pi/wd[1],numpoints=200))[1])[1],COLOR(RGB,1,0,0)),CURVE
S(op(op(plot(eval(1.01*y,[A0=1,L=0.002,C=22*1E-
9,R=1000,w0=wd[i]]),t=-
Pi/wd[1]..Pi/wd[1],numpoints=200))[1])[1],COLOR(RGB,0,0,0)),TEXT(
[0,0.2],cat("w0=",convert(wd[i],string)),FONT(HELVETICA,8))),i=1..
.nops(wd))),AXESLABELS("t","e(t),y(t)'),TITLE("Forma de unda a
semnalelor excitatie (rosu) si raspuns (negru)");
INTERFACE_PLOT(ANIMATE(seq([op(plot([eval(e,[A0=1,w0=wd[i]]),eval
(y,[A0=1,L=0.002, C=22*1E-9, R=1000,w0=wd[i]]),t=-
Pi/wd[i]..Pi/wd[i],color=black))[1],TEXT([0.2,0.2],cat("w0=",con
vert(wd[i],string)),FONT(HELVETICA,8))),i=1..nops(wd))),AXESLABEL
S("e(t)","y(t)'),TITLE("Figura Lissajoux"));
```

Forma de unda a semnalelor excitatie (rosu) si raspuns (negru)

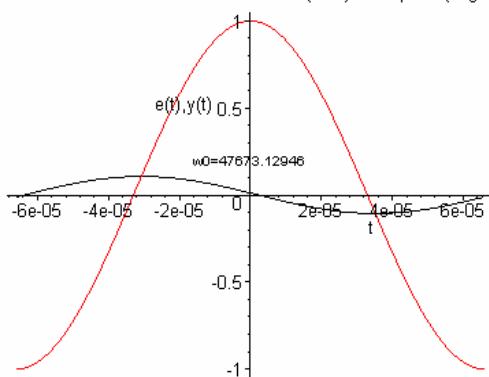
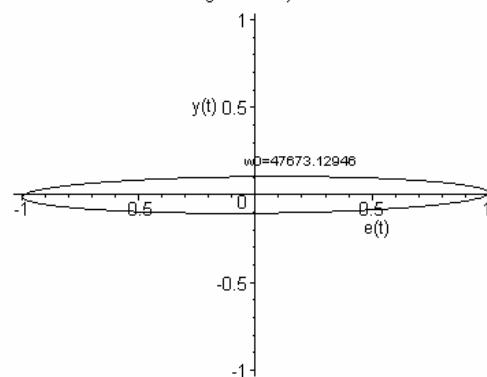


Figura Lissajoux



Raspuns de regim tranzitoriu

Pentru calculul raspunsului tranzitoriu se prefera efectuarea calculelor in domeniul variabilei complexe "s" :

- 1) $e(t) \rightarrow E(s) = L\{e(t)\}$
- 2) $Y(s) = E(s)H(s)$
- 3) $y(t) = L^{-1}\{Y(s)\}$

```
> restart:libname:="c://maple//SCSlib",libname:
> L:=table([dir=inttrans[laplace],inv=inttrans[invlaplace]]):
```

```
>assume(_alpha,positive):assume(_omega,positive):assume(_tau,positive):assume(_T,positive):Hs:=(2*alpha*s)/(s^2+2*alpha*s+omega0^2);
);
Hs := 2  $\frac{\alpha s}{s^2 + 2 \alpha s + \omega_0^2}$ 
```

Raspunsul la semnal treapta (functia pondere)

In acest caz expresia excitatiei $e(t)$ este de forma:

```
> e:=A0*Heaviside(t);
e := A0 Heaviside (t)
```

- Transformata Laplace a excitatiei $e(t)$ este:

```
> E:=L[dir](e,t,s);
```

$$E := \frac{A0}{s}$$

- Transformata Laplace a excitatiei $y(t)$ este:

```
> Y:=Hs*E;
```

$$Y := 2 \frac{\alpha A0}{s^2 + 2 \alpha s + \omega_0^2}$$

- Raspunsul $y(t)$ al circuitului la excitatia $e(t)$ este:

```
> y:=L[inv](Y,s,t)*Heaviside(t);
```

$$y := 2 \alpha A0 \left(-\frac{1}{2} \frac{e^{(-(\sqrt{\alpha^2 - \omega_0^2} + \alpha)t)}}{\sqrt{\alpha^2 - \omega_0^2}} + \frac{1}{2} \frac{e^{((\sqrt{\alpha^2 - \omega_0^2} - \alpha)t)}}{\sqrt{\alpha^2 - \omega_0^2}} \right) \text{Heaviside}(t)$$

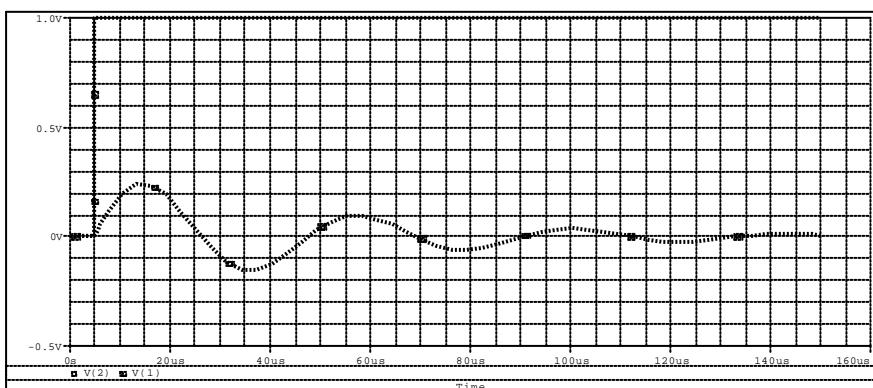
Modificarea functiei pondere la variatia pozitiei polilor

$$e(t) = A\mathbf{s}(t), \quad E(s) = \frac{A}{s}, \quad Y(s) = H(s)E(s) = \frac{2\mathbf{a}A}{s^2 + 2\mathbf{a}s + \mathbf{w}_0^2} \quad \text{unde} \quad \begin{cases} 2\mathbf{a} = \frac{1}{RC} \\ \mathbf{w}_0^2 = \frac{1}{LC} \end{cases}$$

In functie de pozitia polilor distingem urmatoarele 3 cazuri:

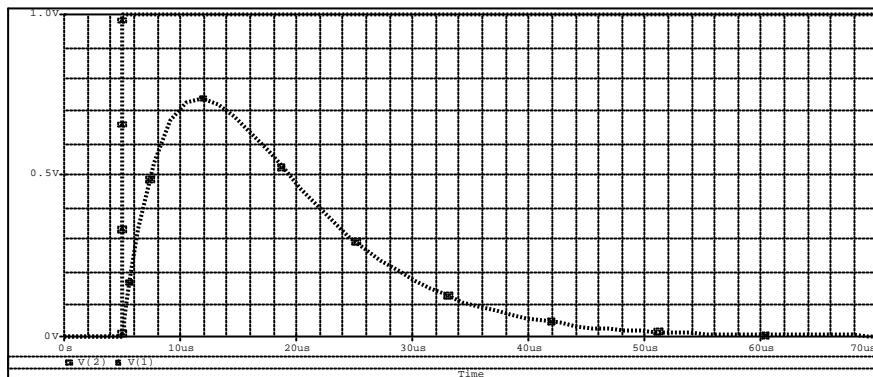
- 1) $\mathbf{a} < \mathbf{w}_0$, $\Delta < 0 \Rightarrow$ poli complex conjugati ($Q > \frac{1}{2}$)

$$Y(s) = \frac{2\mathbf{a}A}{(s + \mathbf{a})^2 + \mathbf{w}_r^2} \quad \text{unde } \mathbf{w}_r = \sqrt{\mathbf{w}_0^2 - \mathbf{a}^2} \quad y(t) = \frac{2\mathbf{a}A}{\mathbf{w}_r} e^{-\mathbf{a}t} \sin(\mathbf{w}_r t) \mathbf{s}(t)$$



2) $a = w_0$, $\Delta = 0 \Rightarrow$ radacini reale egale duble ($Q = \frac{1}{2}$)

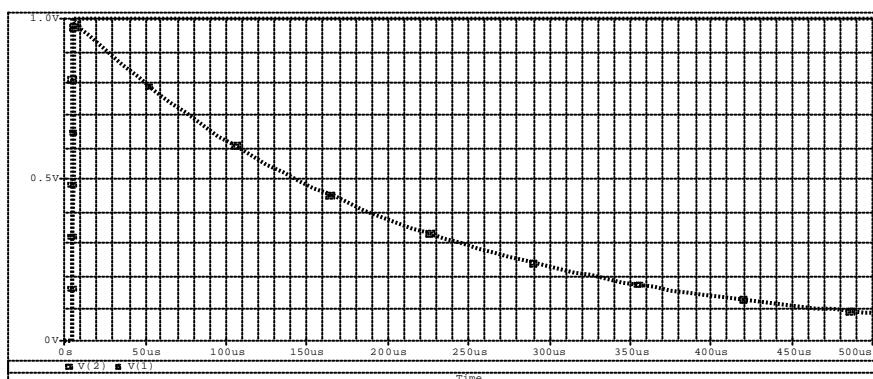
$$Y(s) = \frac{2aA}{(s+a)^2} \quad y(t) = 2aAte^{-at} \mathbf{s}(t)$$



3) $a > w_0$, $\Delta > 0 \Rightarrow$ radacini reale distincte ($Q < \frac{1}{2}$)

$$Y(s) = \frac{k_1}{s + a_1} + \frac{k_2}{s + a_2}$$

$$y(t) = (k_1 e^{-a_1 t} + k_2 e^{-a_2 t}) \mathbf{s}(t)$$



Simulare SPICE a circuitului

```
*Filtru Trece Banda de ordin 2
Vin 1 0 1 AC 1
R1 1 2 {R}
c1 2 0 22nF
L1 2 0 2mH
.PARAM R=10k
.STEP PARAM R LIST 10 150 1k
.PROBE
.AC DEC 100 10Hz 20MEGHz
.END
```

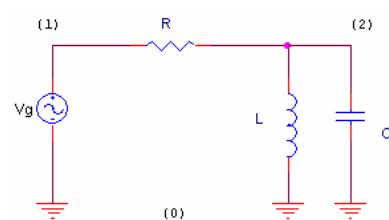
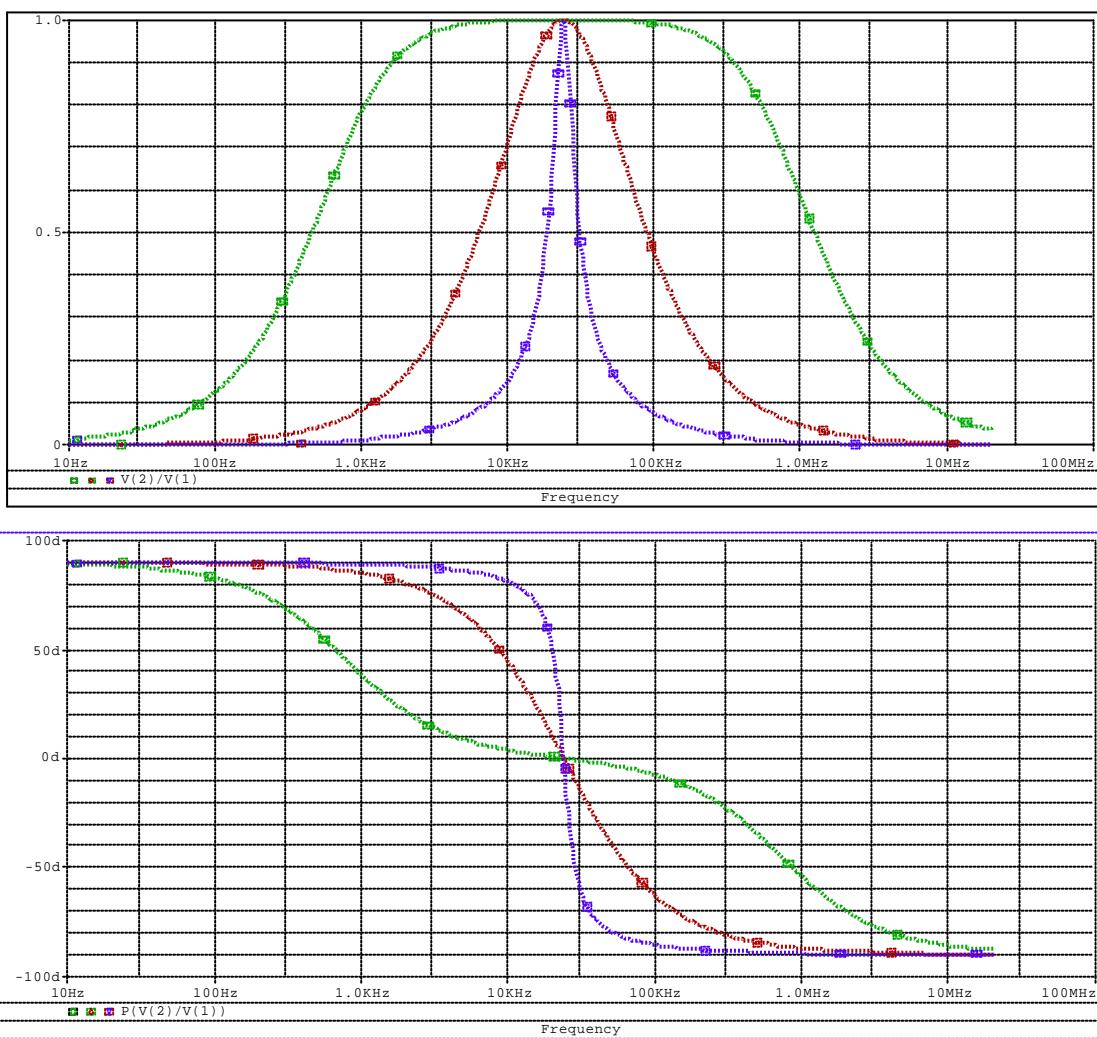


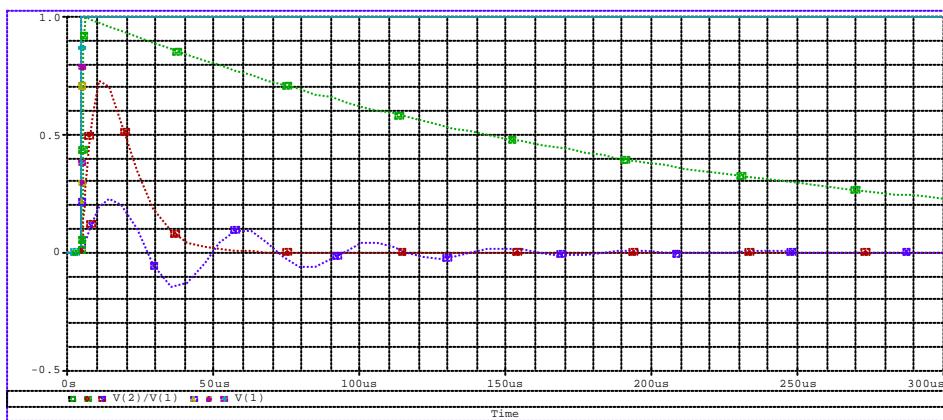
Diagrama Bode de modul si faza

S-au trasat pe acelasi grafic pentru mai multe valori ale rezistentei R: R=10O (verde), R=150O (rosu) si R=1kO (albastru).



Raspuns tranzitoriu

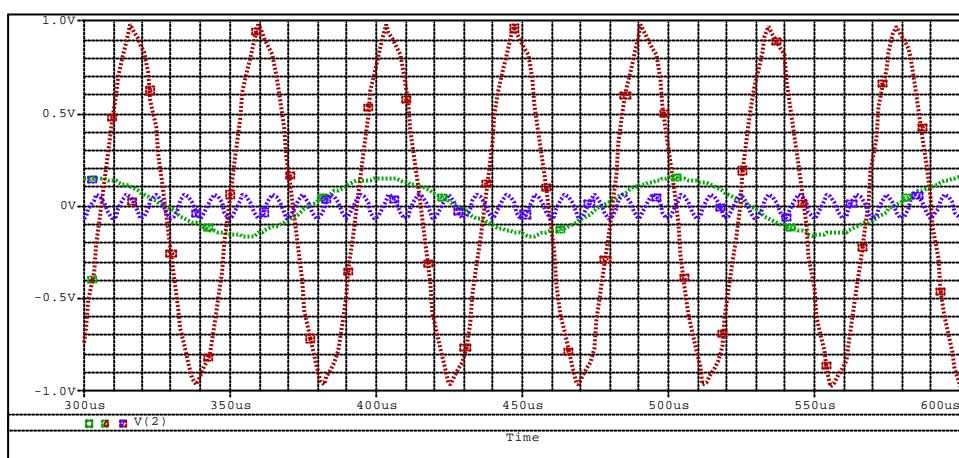
Pentru aceleasi valori ale rezistentei s-a calculat h(t) - functia pondere a circuitului:



Raspuns permanent

Pentru circuitul cu $R=1k\Omega$ se aplica la intrare semnal sinusoidal de frecventa: $f=10\text{KHz}$ (verde), $f=22.9\text{KHz}$ (rosu) si $f=100\text{KHz}$ (albastru). Se vizualizeaza semnalul de iesire dupa ce regimul tranzistoriu s-a stins:

```
* Filtru Trece Banda de ordin 2
Vin 1 0 1 SIN(0 1 {frecv})
R1 1 2 1k
c1 2 0 22nF
L1 2 0 2mH
.PARAM frecv=100khz
.STEP PARAM frecv LIST 10k 22.9k 100k
.PROBE
.TRAN 0.0001n 600u
.END
```

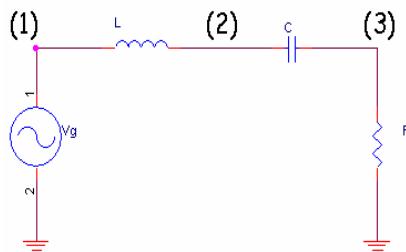


Circuit rezonant - LC serie

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Scopul lucrarii

In lucrarea de fata ne propunem analiza unui circuit liniar de tip Trece Banda (TB) de ordinul II cu grupare serie bobina si condensator. Schema circuitului este:



Caracterizarea circuitului

: Descrierea circuitului folosind un netlist de tip spice

```
> restart:with(Syrup):
> FTB := 
"filtru trece banda
Vg 1 0
L 1 2
C 2 3
R 3 0
.end":
```

Ecuatii de stare

```
> restart:with(Syrup):FTB := "filtru trece banda\nVg 1 0\nL 1
2\nC 2 3\nR 3 0\n.end":
```

Descrierea folosind ecuatii de stare a circuitului

1) **ecuatie de stare (vectorial):**

```
> syrup(FTB, tran, 'currenti','tensiuni');
```

```
Syrup/parseddeck: Analyzing SPICE deck "filtru trece banda" (ignoring this
line)
```

$$\left\{ \frac{\partial}{\partial t} i_L(t) = -\frac{-Vg + i_L(t)R + v_C(t)}{L}, \frac{\partial}{\partial t} v_C(t) = \frac{i_L(t)}{C}, v_C(0) = 0, i_L(0) = 0 \right\},$$

$$\{ i_L(t), v_C(t) \}$$

2) ecuatii de iesire se pot scrie in functie de tensiunile de noduri si curentii prin laturi:

> **tensiuni;**

$$\{ v_3 = i_L(t)R, v_2 = i_L(t)R + v_C(t), v_1 = Vg \}$$

> **curenti;**

$$\{ i_{Vg} = -i_L(t), i_C = i_L(t), i_R = i_L(t), i_L = i_L(t) \}$$

Obs: Ordinul circuitului este egal cu 2. Descrierea functionarii circuitului se face cu un sistem de 2 ecuatii diferențiale de ordin I. Variabilele de stare sunt: tensiunea pe condensator si curentul prin bobina. In functie de aceste variabile se exprima curentii si tensiunile din circuit.

Ecuatii TTN

> **restart:with(Syrup):FTB := "filtru trece banda\nVg 1 0\nL 1
2\nC 2 3\nR 3 0\n.end":**

Descrierea circuitului folosind Teorema Tensiunilor Nodale:

> **syrup(FTB, ac, 'curenti','tensiuni');**

Syrup/parsedeck: Analyzing SPICE deck "filtru trece banda" (ignoring this line)

> **tensiuni;**

$$\{ v_2 = \frac{Vg(sCR+1)}{s^2LC+sCR+1}, v_3 = \frac{sCVgR}{s^2LC+sCR+1}, v_1 = Vg \}$$

> **curenti;**

$$\begin{aligned} \{ i_L &= \frac{sCVg}{s^2LC+sCR+1}, i_{Vg} = -\frac{sCVg}{s^2LC+sCR+1}, i_C = \frac{sCVg}{s^2LC+sCR+1}, \\ i_R &= \frac{sCVg}{s^2LC+sCR+1} \} \end{aligned}$$

Calculul functiei de transfer H(s)

Metoda I: divizor rezistiv

Calculul functiei de transfer folosind divizor de tensiune:

$$H(s) = \frac{\frac{1}{sC}}{R + sL + \frac{1}{sC}} = \frac{\frac{R}{L}}{s^2 + s\frac{R}{L} + \frac{1}{LC}}$$

Notam:

$$2a = \frac{R}{L}, \quad w_0^2 = \frac{1}{LC}$$

Deci functia de transfer devine:

$$H(s) = \frac{2as}{s^2 + 2as + w_0^2}$$

Se defineste factorul de calitate :

$$Q = \frac{w_0}{2a}$$

Circuit rezonant LC

In cazul nostru factorul de calitate este:

$$Q = \frac{1}{R} \sqrt{\frac{L}{C}}$$

Se calculeaza polii si zerourile functiei de transfer.
zero

$$z = 0$$

poli:

$$p_1 = -a - \sqrt{a^2 - w_0^2}$$
$$p_2 = -a + \sqrt{a^2 - w_0^2}$$

In functie de factorul de calitate Q avem doua cazuri:

Cazul I ($Q < \frac{1}{2}$ respectiv $R > 2\sqrt{\frac{L}{C}}$) avem doi poli reali distincti.

Cazul II: ($Q = \frac{1}{2}$ respectiv $R = 2\sqrt{\frac{L}{C}}$) avem un pol dublu.

Cazul III ($Q > \frac{1}{2}$ respectiv $R < 2\sqrt{\frac{L}{C}}$) avem poli complexi conjugati.

Metoda II: ecuatii TTN

Pentru circuitul cu nodurile din figura se scrie TTN:

$$\begin{cases} V_{10}(s) = Vg(s) \\ -\frac{1}{sL}V_{10}(s) + \left(sC + \frac{1}{sL}\right)V_{20}(s) - sCV_{30}(s) = 0 \\ -sCV_{20}(s) + \left(sC + \frac{1}{sL}\right)V_{30}(s) = 0 \end{cases}$$

Rezolvind acest sistem ajungem la acelasi rezultat.

Metoda III: calcul simbolic

```
> restart:with(Syrup):FTB := "filtru trece banda\nVg 1 0\nL 1  
2\nC 2 3\nR 3 0\n.end":  
> libname:="c://maple//SCSlib",libname:  
> syrup(FTB, ac, 'currenti','tensiuni'):  
Syrup/parseddeck: Analyzing SPICE deck "filtru trece banda" (ignoring this  
line)  
> Hs:=eval(v[3]/v[1],tensiuni);  

$$Hs := \frac{s C R}{1 + s C R + s^2 C L}$$
  
> Hs:=sort(simplify(eval(Hs,[C=(2*alpha)/(omega0^2*R),  
L=R/(2*alpha)])),s);  

$$Hs := 2 \frac{\alpha s}{s^2 + 2 \alpha s + \omega_0^2}$$

```

Evaluare numerica:

```
> alpha:=R/(2*L):omega0:=1/sqrt(L*C):
> H:=eval(Hs,[L=0.002, C=22*1E-9, R=700]):
```

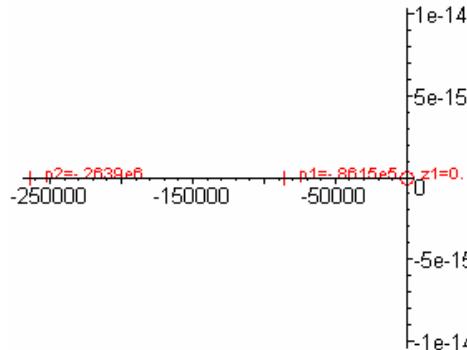
Polii si zerourile functiei de transfer:

```
> PZ[numeric](H,s);
```

$$\begin{bmatrix} zI & 0. \\ p1 & -86150. \\ p2 & -263900. \end{bmatrix}$$

```
> PZ[grafic](H,s);
```

Diagrama poli-zerouri



```
> plot3d(abs(eval(H,s=sigma+I*omega)),sigma=-400000..400000,omega=-400000..400000,numpoints=2500,axes=normal,title="Reprezentarea in spatiu a modulului F.D.T.");
plot3d(argument(eval(H,s=sigma+I*omega)),sigma=-400000..400000,omega=-400000..400000,numpoints = 2500, axes=normal,
title="Reprezentarea in spatiu pentru argumentul F.D.T.");
Reprezentarea in spatiu a modulului F.D.T.
```

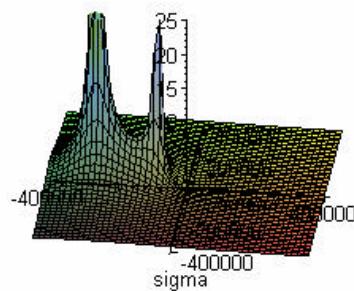


Diagramme frecventiale

```
> restart:libname:="c://maple//SCSlib",libname:
> Hs:=(2*alpha*s)/(s^2+2*alpha*s+omega0^2);
```

$$Hs := 2 \frac{\alpha s}{s^2 + 2 \alpha s + \omega_0^2}$$

```
> alpha:=R/(2*L):omega0:=1/sqrt(L*C): cat("omega0 = ",convert(eval(omega0,[L=0.002, C=22*1E-9, R=700]),string)," rad/s");
"omega0 = 150755.6723 rad/s"
```

```
> Bode[castig](eval(Hs,[L=0.002, C=22*1E-9, R=700]),numarpunche=400);Bode[faza](eval(Hs,[L=0.002, C=22*1E-9, R=700]),numarpunche=400);
```

Diagrama Bode de castig

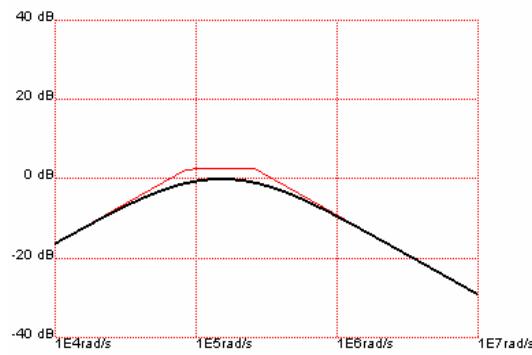
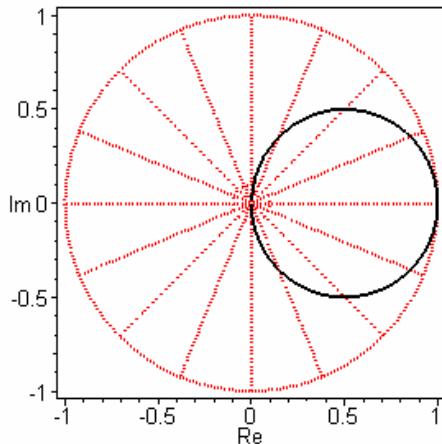


Diagrama Bode de faza

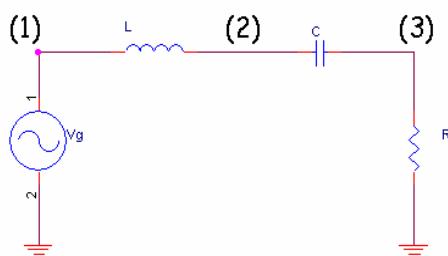


```
> Bode[polar](eval(Hs,[L=0.002,C=22*1E-9,R=700]),numarpunche=400);
```

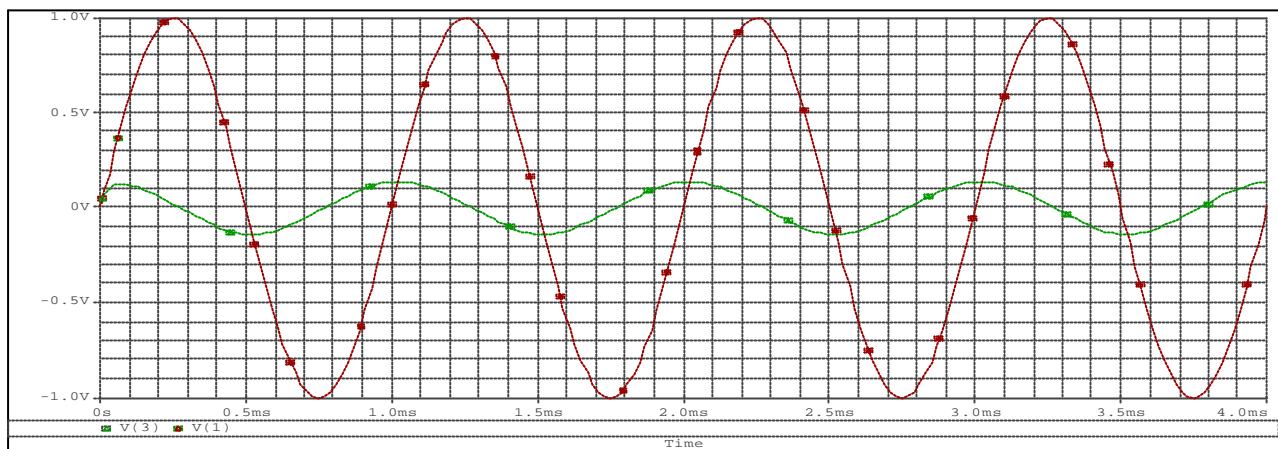
Diagrama polara



Simulare Spice



```
*FTB
Vg 1 0 SIN(0 1 1KHz)
L 1 2 0.0001
C 2 3 22n
R 3 0 1K
.tran 0.1m 4m 0 20u
.probe
.end
```



Functia pondere la variatia rezistentei R

```

*FTB
Vg 1 0 PULSE(0 1 1n 1n 0 600u 601m )
L 1 2 2m
C 2 3 22n
R 3 0 {R}
.PARAM R=10K
.STEP PARAM R LIST 100 603 1K
.PROBE
.TRAN 0.0001n 600u
.END

```

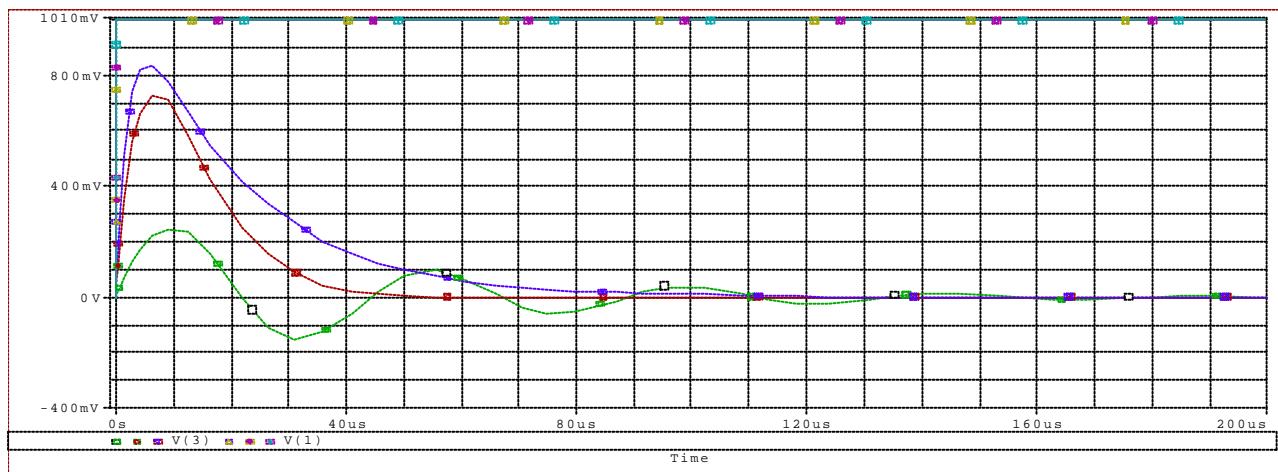


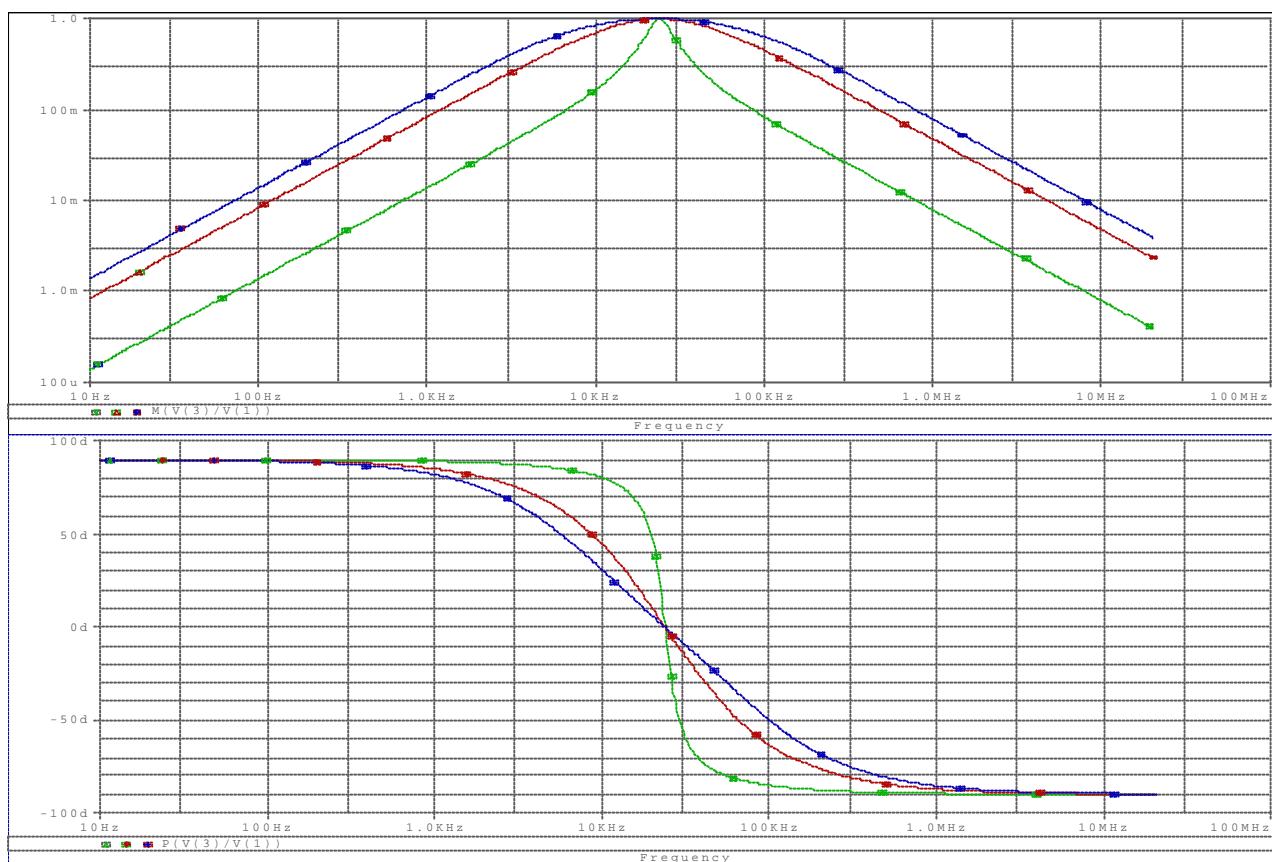
Diagramme Bode de modul si faza la variatia rezistentei R

```

*FTB
Vg 1 0 AC 1
L 1 2 2m
C 2 3 22n
R 3 0 {R}
.PARAM R=10K
.STEP PARAM R LIST 100 603 1K
.AC DEC 100 10Hz 20MEGHZ
.probe
.end

```

Circuit rezonant LC



Comportarea circuitului la variația lui R (pozitia poli-zerouri, diagramele Bode, funcția pondere)

Modul	Faza	Rasp. Transistoriu
Polii-Zerouri	Diagrama poli-zerouri	Diagrama poli-zerouri
	$+ p_1 = -25000e5 + 1487e6j$ $+ p_2 = -25000e5 - 1487e6j$	$\Sigma = 0.002, C = 22 * 1E-9, R = 100$ $\Sigma = 0.002, C = 22 * 1E-9, R = 603$ $\Sigma = 0.002, C = 22 * 1E-9, R = 1k$
Maple		